Barney oliver AMPLIFIER

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# SECTION I <br> DESCRIPTION 

## A. GENERAL

The Barney Oliver Amplifier is a high quality all solid state audio amplifier designed for two channel stereo sound reproduction in the home, in studios, and in small to medium sized auditoriums. It is intended for use with full frequency range 8 to 16 ohm speaker systems and with signal sources (phonograph pickups, tape decks, AM and FM tunners) that are themselves flat enough to require little or no equalization. In addition to the power amplifiers, the unit includes phono preamplifiers designed to operate from any of several magnetic phono cartridges. These preamplifiers provide the necessary equalization for the RIAA recording characteristic. Additional plugin preamplifier boards have been designed for direct moving coil microphone input or for direct input from low-level, high impedance sources. Adding this feature will require that the user build the preamplifier boards, install and wire printed circuit connectors in the deck, drill front or rear panel holes as required, and modify selector switch wiring.

Hum and distortion are inaudible. As a result of careful attention to filtering and to lead routing on printed circuit boards, the residual hum is well below thermal noise (which itself has been minimized by optimum input stage design). The output stages of the amplifiers are operated class-B to reduce standby power drain and are biased and locally degenerated to reduce crossover distortion. A large amount of overall negative feedback, ranging from over 100 dB loop gain at dc and low frequencies to over 50 dB at the top of the audio range further reduces any remaining harmonic and inter-modulation distortion. Since the
$\mu$-circuits are direct coupled, overload produces no long time constant transients; the peaks are simply clipped and the original waveform resumes at its proper value immediately afterward. Because of the large amount of feedback, signals only a fraction of a dB below actual overload typically show a total distortion over 75 dB below the fundamental.

Bridged-tee networks in the $\beta$-circuits of the amplifiers, and active filters in the mixing and control board, enable the low-end response to be maintained down to 20 Hz and to fall off very rapidly below the audible range. This prevents the amplifier and loudspeakers from being driven beyond their linear excursions by low frequency transients arising from such sources as warped records or breath blasts into microphones. The high end response is reduced at 18 dB per octave above 20 kc by another pair of active filters to protect the amplifiers against overload by, or rectification of, strong r-f signals.

The power amplifiers are protected against damage from accidental short-circuits at their outputs. Momentary shorts will have no effect, but sustained shorts may blow one or more of the protective fuses. In addition, all power supply outputs are either current limited or fused so that shorts from test probes will in general cause no damage.

Finally, considerable effort was devoted to reducing switching transients. A balanced build-up and decay of power supply voltages and careful balancing of function drops minimizes the turn-on transients in the amplifiers. A slow turn-on in the low voltage regulated supplies further reduces the turn-on transient from the pre-amplifiers.

## SPECIFICATIONS

## OUTPUT PER CHANNEL

| SPEAKER $Z$ | CONTINUOUS* |  | AUDIO PEAK |
| :---: | :---: | :---: | :---: |
| 16 |  | $\approx 36 \mathrm{~W}$ |  |
| 8 |  | $\approx 50 \mathrm{~W}$ |  |
| 4 |  | $* *$ | $\approx 160 \mathrm{~W}$ |
|  |  |  | $\approx 80 \mathrm{~W}$ |

## HARMONIC DISTORTION

$<0.01 \%, 2 \mathrm{mw}$ to max. power, all freqs.

## HUM AND NOISE

Power Amplifier: 100 db below max. output $\dagger$ Phono Preamp: 84 db below one volt output

## INPUT VOLTAGE FOR FULL OUTPUT

Tuner, Tape, Aux 1, Aux 2: $\leq 1.0$ volt rms Phono: $\leq 5 \mathrm{mv} \mathrm{rms}$

## IINPUT IMPEDANCE

Tuner, Tape, Aux 1, Aux 2: $100 \mathrm{~K} \Omega$
Phono: Optimized for SHURE V-15 Type II Pickup.

## CONTROLS

INPUT: TUNER, TAPE, PHONO, AUX 1, AUX 2.

MODE:
STEREO - DIR(ect), REV(erse), L, R MONO - DUAL, L, R

[^0]
## FREQUENCY RESPONSE



## CONTROLS (Cont'd.)

FILTER: Controls active h.f roll-off filter $>18 \mathrm{~dB}$ /octave with corner at $5,8,10$ or 20 kHz . Includes 30 dB notch at 10 kHz in 5 and 8 kHz positions.

VOLUME: Dual precision attenuator, 60 dB range, 2 dB steps. Eliminates need for balance control.

BASS: FLAT, BOOST
Response: RIAA, $+6 \mathrm{~dB},-6 \mathrm{~dB}$

## SIZE:

16.72 " ( 425 mm ) wide, $5.0^{" ~(127 ~ m m) ~ h i g h, ~}$ $10.93^{\prime \prime}(278 \mathrm{~mm})$ deep behind panel.

## WEIGHT

Approximately 20 pounds net without case.

## POWER REQUIREMENTS

115 or 230 V.A.C. $\pm 10 \%, 50-60 \mathrm{~Hz}, 20 \mathrm{~W}$ standby power, 135 W at full output into $16 \Omega$ (both channels).

## SECTION II

## FRONT PANEL CONTROLS

Simplicity of operation has been achieved with a minimum of controls. It is a good idea to mark with a colored dot the "normal" settings of special purpose controls so that the inexperienced or technically naive operator need only check these settings and achieve good results using only the input selector and volume control.

## A. INPUT Selector

This switch allows a choice of any one of five inputs. From left to right these are:

TUNER Accepts input at line level (0 dBm ) from FM , AM, or FM/AM tuner.

TAPE

PHONO Accepts input from a magnetic stereo phonograph pickup.

AUX 1 Accepts inputs from any linelevel audio circuit such as tuners, AUX 2 tape decks or other sources.

## B. MODE Switch

This control allows the left and right channels of the input to be delivered to the speakers in various ways. The center position is normal for stereo operation. From left to right the modes are:

L Left stereo channel only to left speaker.

R Right stereo channel only to right speaker.

REV

DIR
Stereo channels reversed. Left channel to right speaker, right channel to left speaker.

Direct presentation. Each stereo channel to corresponding speaker -Normal position.

DUAL

L Monophonic reproduction of "left" channel over both speakers.

Monophonic reproduction of "right" channel over both speakers.

The L and R positions allow monophonic tapes and other signal sources to be reproduced over either one (STEREO side) or both (MONO side) speakers.

## C. FILTER Switch

This control allows various high frequency roll-offs to be introduced. From left to right the positions are:

5 Introduces a high frequency cutoff at 5 kHz , with a null at 10 kHz . Useful for noisy 78 rpm records and AM reception.

8 Introduces a high frequency cutoff at 8 kHz with a null at 10 kHz . Useful for good 78 rpm records and AM reception.

20
Normal position. Introduces a maximally flat $18 \mathrm{~dB} /$ octave cutoff at 20 kHz .

## D. VOLUME Control

A dual precision attenuator allows adjustment of the sound level in 2 dB (or scarcely perceptible) steps over a 60 dB range. Because the attenuation is precisely balanced and because the feedback assures equal gain in both channels, the nuisance and hazard of an improperly set
balance control are eliminated. (Note: Identical speakers are assumed. Good quality speakers of good manufacture will ordinarily be within 1 dB of each other over the audio range. Likewise for the two channels of a good phono-cartridge. However, the perfectionist may want to test his components and introduce appropriate loss into the "hot" side.)

## E. Phono Equalization Switch (-6 dB, RIAA, +6 dB )

Below the INPUT selector control, and effective only in the PHONO position of that control, a three-position slide switch allows some compensation for recording defects. In the center (Normal) position, this switch provides the standard RIAA equalization. In the left position, the high frequency response is dropped by 6 dB , while in the right position, the response is enhanced by 6 dB . Some manufacturers (such as Deutsche Gramophone) conscientiously adhere to RIAA specifications, while others (names supplied on request)
enhance the high end to compensate for the deficiencies of the usual playback system. If your speakers are flat, the -6 dB position will help correct this practice. If you find the +6 dB position better in the majority of cases, your speakers (or your ears) need attention.

## F. BASS Switch (FLAT, BOOST)

Located below the high frequency FILTER control is the two-position BASS switch. In the BOOST position, the switch raises the response at 6 dB /octave from 80 Hz down to 20 Hz . In the BOOST position, approximate compensation is provided for the usual low-end roll-off of good speakers. (Two poles at $40-50 \mathrm{~Hz}$ ). If you are fortunate enough to have an overdamped pair of woofers with real poles at 80 Hz and 20 Hz (such as LE-15A's or ALTEC 411-A's in 9 cu . ft. or larger enclosures), the BOOST position will closely compensate the low-end roll-off down to the bottom of the audio range. For very high sound levels, the FLAT position is recommended.

## SECTION III

## INSTALLATION

## A. PHONO CONNECTIONS

Special precautions must be observed for the PHONO input. Because a combination of shunt and series feedback is used to control the impedance faced by the cartridge and thereby produce the high end roll-off required by the RIAA recording characteristic, the "LOW" side of each input is not grounded inside the amplifier and THESE MUST NOT BE GROUNDED OR CONNECTED TOGETHER externally. (See Section V, A. for further information.) If coaxial or shielded wires are used for each channel, the two inner shields
must be insulated from each other and from the outer shield around both as shown in Figure 1. In some cartridges, the LOW side of one or both channels is grounded to the case by a thin strap at one or both LOW terminals. IF PRESENT, THESE GROUNDING STRAPS MUST BE REMOVED BY PRYING THEM OUT AND OFF WITH A LARGE NEEDLE OR PICK. The overall shield should be connected to the turntable frame at one end and to the amplifier chassis at the other end using the binding post provided. After this is done, test that both channels are isolated from ground before connecting them to the amplifier.


NOTE:

Inner shields must not be grounded at either end. Also inner shields must not be connected together at any point (including at or inside pickup). Cables should have insulation over shields.

Outer shield must not make contact with any
lead connecting pickup to amplifier (including inner shields).

In some locations the outer shield may not be necessary; in such cases, turntable or changer chassis should be connected to amplifier chassis (ground terminal on rear) with a separate wire, preferably insulated.

Figure 1. Phono Connections

The phono cartridge should be located as far as is convenient from any transformers, motors, or other source of AC magnetic field. With proper installation and a good cartridge, no AC hum should be audible even at the full setting of the volume control and with bass boost.

## B. USE OF PHONOGRAPH PICKUPS OTHER THAN SHURE V15 TYPE II

The phonograph pre-amplifiers as shipped are optimized for the Shure V15 Type II pickup. Other good quality pickups can be used, but a resistor change on each of the phono pre-amp boards may be required. The resistors in question are designated R1 as shown near the left side of the pre-amp schematic in Section VI, A. To determine the optimum value for R1 for a given pickup, the inductance and resistance of the pickup must be known. The value for resistor R1 may then be calculated by using the following equation:

$$
R_{1}=\frac{L_{o}}{.75} \times 10^{6}-100 R_{o}-20 \mathrm{~K}
$$

Where $L_{O}$ is pickup inductance in Henries, $R_{O}$ is pickup internal resistance in ohms, and $\mathrm{R}_{1}$ is in ohms.

Once the value for R 1 has been calculated, R1 resistors on each of the two phono pre-amp boards should be changed to the proper value. For additional information, see Section V, A.

## C. SPEAKER CONNECTIONS

The amplifier may be located at any convenient distance from the loudspeakers. Twisted pairs of No. 18 wire or larger or ordinary zip-cord may be used to connect the amplifiers to the speakers if the distance is under 100 feet. For longer distances, heavier conductors are recommended. In general the d-c resistance of the cables or cords should not exceed $5 \%$ of the speaker impedance.

Connection to the amplifier outputs is via the two-terminal polarized Jones sockets at the rear of the amplifier. The cords or cables must be soldered to the mating plugs provided, taking care to avoid internal short circuits from wire strands or solder bridges. It is good practice to insulate the wire and lugs from each other with electrical tape or heat shrinkable tubing inside the plug sleeve after soldering.

## D. SPEAKER PLACEMENT

The loudspeakers should be located at the ends of the base of an isosceles triangle with the listener at the apex. The apex angle of this triangle, i.e., the angle between the lines of sight to the two speakers should be about $15^{\circ}$ to $45^{\circ}$, as shown in Figure 2. Good sound quality will then be heard up to $45^{\circ}$ on either side of the perpendicular bisector of the line between the speakers.


## E. LINE VOLTAGE, FREQUENCY AND LINE FUSING

Unless specifically tagged otherwise, amplifiers operate only on 115 V ac line. 115 V amplifiers have single power transformer primaries and cannot be connected for 230 V operation. (An external $230-115 \mathrm{~V}$ step-down transformer may be used.) The proper line fuse for 115 V units is 1.6 amp , slow-blow.

Satisfactory operation will be obtained with line voltages within $\pm 10 \%$ of the nominal $(115 \mathrm{~V}$ or 230 V ) value. The line frequency should be 50 Hz or greater. A grounding or three wire socket is recommended but not essential. If the chassis is not grounded through the power cord, a separate ground may be needed to get rid of hum on phono, mike or other low level inputs.

## F. $115 \mathrm{~V} / 230 \mathrm{~V}$ AVIPLIFIERS (European Units)

Units shipped to Europe (and in a few cases within the United States) are equipped with $115 / 230 \mathrm{~V}$ power transformers.

Units shipped to Europe will be connected for 230 V operation and will be equipped with 0.8 amp slow-blow fuses. Because of the variety of ac plugs used, amplifiers shipped to Europe will not include line cords. The line connector on the rear of the amplifier is compatible with European line cords, and it is assumed that the user can obtain the proper cord. Units connected for 230 operation will be prominently tagged.
$115 / 230 \mathrm{~V}$ amplifiers shipped within the United States will be connected for 115 V operation, will use 1.6 amp slow-blow fuses, and will be equipped with standard line cords. These units will be tagged to indicate $115 / 230$ capability.

Amplifiers with $115 / 230 \mathrm{~V}$ power transformers may be reconnected by the user for either line voltage. 115 V operation requires connecting the two halves of the transformer primary in parallel; for 230 V , the two halves must be connected in series.

> --NOTE-

When reconnecting transformer primaries, care must be taken to insure that windings are connected in an "aiding sense" (instantaneous flux produced by both windings must have the same polarity).

The line fuse must be changed when changing the line voltage ( 1.6 amp for 115 V ; 8 amp for 230V).

## G. INSTALLING AMPLIFIER IN AN EXISTING CABINET

If the amplifier is to be installed in an existing cabinet, careful attention should be paid to the outline drawing shown in Section III, J. Because certain components, especially the power supply capacitors, are quite large, it will be seen that the overhang at the top of the front panel is not very great and at the bottom edge is virtually zero. This will require considerable care in cutting the necessary hole in the cabinet. It is strongly recommended that the amplifier be examined in detail before laying out this hole to prevent costly mistakes. Referring to the side view in the outline drawing in Section III, J., it will be seen that overall front panel height is $5^{\prime \prime}$, that the rear panel height is $4.85^{\prime \prime}$, and that the side gussets are $4.48^{\prime \prime}$ high. This will make possible the use of a hole somewhat less than $4.85^{\prime \prime}$ high, if the amplifier can be tipped slightly as it is inserted.

Front panel overhang at each side is approximately $1 / 4 /$ ", requiring less precision in the horizontal dimension.

## H. ASSEMBLY OF WALNUT OR TEAK ENclosure

If the walnut or teak enclosure option was included with your amplifier, it may be assembled as outlined below. (See Section III, J. for picture of assembled enclosure.)

The enclosure kit consists of the following:
Two wood side panels (one right and one left).
Black vinyl-clad aluminum top cover with retaining screw.

Four 10-32 flat-head Allen screws and nuts for attaching side panels to amplifier.

Wood side panels have been sanded but not finished. It is recommended that the wood pieces be finish sanded with fine sandpaper such as 400 or 600 grit. They can then be finished as you please. One quick, simple and beautiful finish which can be done by most anyone anywhere is an oil finish, with or without stain. Most paint stores and many hardware stores sell Danish oil finish materials (one brand is Watco).

If a high-gloss finish is desired, it will be necessary to apply filler to the wood before staining and applying finish. For this process the user is referred to his friendly paint store or cabinet shop.

## ASSEMBLY INSTRUCTIONS

Attach the wood side panels to the amplifier with the Allen screws and nuts. It will be noted that the side panels are notched across one end to clear the front panel overhang and to allow the wood panel to extend slightly forward of the front panel. Near one edge of each wood panel is a slot extending the full length. The panel should be attached so that these slots are at the top of the amplifier and face inboard.

The aluminum top cover slides into the slots just mentioned, with the front edge fitting into a slot at the top rear of the front panel.

The rear edge of the top cover lies on the top of the back panel and is secured with a single
screw through the top cover. It may be necessary to adjust the positions of the wood side panels to permit the top cover to slide into place without interference from side gussets or other amplifier parts.

## I. RACK MOUNTING CABINET

If your amplifier was furnished in an HP type cabinet, it can be rack mounted by use of the standard rack mount kit shipped with the instrument. Instructions are included with the kit.

## J. PICTURES AND OUTLINE DRAWING

(See following page.)


## SECTION IV <br> LOUDSPEAKER PHASING

Proper stereo reproduction requires that the loudspeakers be properly phased. To check this, insert a reversing switch in the leads to one speaker as shown in Figure 3. Turn on the power and the signal sources and bring up the volume. Set the MODE switch to "DUAL". Station yourself exactly midway between the speakers and about three feet in front of the plane of their front baffles. Try reversing the switch. In the proper position the sound should appear to originate from dead ahead of you. In the improper position this illusion disappears and both sources are heard independently. Unless the speakers are matched, the above test is difficult, but with identical speakers the illusion is very striking and the test is easy to perform. Reconnect the speaker pre-
serving the proper polarity. This test need only be done once. Return the MODE switch to the normal STEREO-DIRECT position.

If, on the average, one channel seems louder than the other, throw the MODE switch to the STEREO-REVERSE position. If the loud channel shifts to the opposite speaker the signal source or program material is defective. If the loud channel stays with the same speaker, the other speaker is less efficient. If the speakers are supposedly identical, the weak one may be defective. (Check the d-c resistance of the speakers. These should be the same within $5 \%$.) The use of different speakers for the two channels is not recommended.


Figure 3.

# SECTION V CIRCUIT DESCRIPTIONS 

## A. PHONO-PRE-AMPLIFIER

The phono pre-amplifier uses a combination of series and shunt feedback to the input terminals to provide a resistive input impedance of the proper value to produce, together with the self inductance of the pickup, the required RIAA high frequency roll-off above 2120 Hz . If $\mathrm{L}_{\mathrm{O}}$ is the pickup inductance and $R_{o}$ the resistance, and if $R$ is the input resistance to the pre-amp we require that

$$
\frac{\mathrm{L}_{\mathrm{O}}}{\mathrm{R}+\mathrm{R}_{\mathrm{O}}}=75 \times 10^{-6} \text { seconds }
$$

This leads to the value of R 1 given in the schematic. As supplied, R1 is appropriate for the Shure V-15 Type II cartridge. To provide the $\pm 6 \mathrm{~dB}$ variation of high end response, the shunt feedback is halved or doubled.

The series feedback is applied to the low end of the pickup windings which places these ends (normally the outer shields of coaxial lines) $10 \Omega$ above ground. To avoid hum and RF pickup it is recommended that an outer shield insulated from both inner shields be used. This shield should connect the record player frame to the amplifier chassis.

A balanced differential stage is used at the input to avoid drift and $R F$ rectification. The remainder of the amplifier is similar to the power amplifier except for power level. The output Class B stage can supply a $600 \Omega$ line or headphones at line level ( 0 dBm ) without appreciable distortion.

The low end bass boost of the RIAA characteristic below 500 Hz is provided by C12 and R3 $+\mathrm{R} 4+\mathrm{R} 5+\mathrm{R} 6$ and R 28 . The low end cutoff is provided by C2 and C3 together with C4, C5 and R10. This combination provides unity d-c external gain and a fourth order maximally flat low-end cutoff at about 16 to 20 Hz .

Great care was used to make the projected area of the input circuit zero in all directions by properly routing the conductors and by providing the loops shown. This minimizes the magnetic coupling to the power transformer and reduces the hum below audibility. (If you notice any hum, it's from coupling directly to the cartridge.)

Because the input impedance is low (about $10 \mathrm{~K} \Omega$ ) cable capacitance has no effect on the high end response for lengths up to 10 or 20 feet depending on the cable used.

Many of the components that may puzzle you, such as Q3 or CR8 or such as CR1, CR2, CR5, etc., are there to avoid turn on transients or avoid emitter base breakdown. Everything has a function, but invincible fatigue prevents me from going into all the gory details.

## B. FILTER BOARD

The filter board provides a sharp low-end cutoff below 16 Hz to protect the speakers against large useless cone exursions, and a controllable high-end cutoff to suppress the high frequencies with noisy or distorted program material.

The board contains four unity gain amplifiers consisting of two cascaded emitter followers (example: Q3 and Q5) with constant current supplies (example: Q1 and Q7). This combination provides very high input impedance, very low output impedance and low distortion.

The two input unity gain amplifiers are coupled to the input selector switch through active high pass filters that drop rapidly in transmission below 16 Hz (example: $\mathrm{C} 1, \mathrm{R} 1, \mathrm{C} 3, \mathrm{R} 7, \mathrm{Q} 3, \mathrm{Q} 5$ ). The output of these feed the mode selector switch.

The output unity gain amplifiers provide drive for the dual precision volume control and are coupled to the mode selector switch via active low-pass filters. These are three pole filters, two of the poles being provided by the input $R C$ networks and the remaining poles (and zeros) by the shunt branch at the output.

Potentiometers are provided to supply the base currents of the input emitter followers and thereby enable the voltages at terminals $5,4,20$ and 21 to be set equal to zero. This eliminates transients when the mode and filter switches are switched.

## C. POWER AMPILIFIER

The output stage of the power amplifier is a cascaded complementary emitter follower comprising transistors Q12* and Q13*, with Q10 and Q11 as their drivers. Operating point stability is provided by resistors R5* and R6* and by currents from current source Q8 flowing through CR7, CR9, R22, CR8 and CR6. The power diodes CR1* and CR2* shunt $R 5^{*}$ and $R 6^{*}$ at high signal levels to avoid large voltage drops in these resistors. Inductance L1* protects the output stages from the effects of capacitive cable loads at very high frequencies while $R 8 *$ eliminates any series resonance with this capacity. Diodes CR10, CR11, CR12 and CR13 provide output current limitation. Together with fuses $\mathrm{F}^{*}$ these provide output short circuit protection. The output stages are driven by emitter follower Q9, which has current limitation in the collector.

The input stage consists of a differential pair, Q1 and Q2, whose emitter currents are supplied by Q4. The input signal is applied to the base of Q1 and the feedback to the base of Q2. The output collector swing of Q1 is limited by CR2 and CR3 to protect the emitter-base junctions of the second stage comprising Q5 and Q7.

The loop gain at $d-c$ and low frequencies is extremely high ( $>100 \mathrm{~dB}$ ). The primary cutoff for the loop gain at high frequencies is the basecollector capacitance of Q7. Thus the loop gain falls at 6 dB /octave to reach a value of about 60 dB at 10 kHz . Inductors L1 and L2 introduce a second pole at 16 kHz above which the loop gain falls at $12 \mathrm{~dB} /$ octave to about 200 kHz , where C6 begins to shunt R16 producing a high end cutoff in the amplifier and reducing the loop gain cutoff rate to $6 \mathrm{~dB} /$ octave once more. Gain crossover is at about 1 MHz .

The bridged-T comprising $\mathrm{C} 3, \mathrm{C} 4, \mathrm{R} 11$, and R12 increases the loop gain below 16 Hz and reduces the external gain to unity at d-c. The poles in the external gain are slightly complex so the low end response rises slightly at the low end before dropping off. In the bass-boost position C7 and C8 together with R16 and R17 produce a pole at 16 Hz and a zero at 80 Hz in the external gain. Thus the gain rises at $6 \mathrm{~dB} /$ octave below 80 Hz , to compensate for the low end roll-off of most loudspeakers.

[^1]Transistor Q3 supplies current to two potentiometers R4 and R5, which are adjusted so that the currents through R2 and R3 supply the base currents of Q1 and Q2. By adjusting R5 with the input terminals shorted (volume control at minimum) and R4 with the input terminals open (or with the volume control at maximum) to give zero volts out of the amplifier, this condition will hold for any impedance the amplifier faces (any volume control setting).

## D. POWER SUPPLY

All supply voltages ( $50 \mathrm{~V}, 40 \mathrm{~V}, 20 \mathrm{~V}$ and 10 V ) are available in both polarities. The main supply ( $\pm 40 \mathrm{~V}$ ) is rectified by diodes CR1, CR2, CR3, and CR4 in a double full wave configuration. Filtering is by capacitors C3 and C4. This supply has a substantial amount of ripple, especially under load, but the power amplifier by-passing is such that this produces negligible hum in the amplifier output.

## -WARNING-

The terminals and leads of C3 and C4 are not current protected. Do not short to ground or to each other. (You'll ruin your screwdriver.)

The $\pm 50 \mathrm{~V}$ supplies are really 10 V supplies floated on the +40 V supplies respectively. They will show about the same ripple as the latter. Transistors Q1 and Q2 with their associated circuitry provide protective current limits on the $\pm 50 \mathrm{~V}$ supplies.

Zener diodes CR13 and CR14 establish the reference voltages for the $\pm 20 \mathrm{~V}$ supplies obtained from the cascaded emitter followers Q3-Q5, and Q4-Q6. The rate of rise and fall of these supplies during turn on and turn off is determined by the two stage active filters comprising R9, C5, R13 and R15, C7 and transistor Q3 for the +20 V supply and R10, C6, R14 and R16, C8, and transistor Q4 for the -20 V supply. Diode CR17 compensates for junction drops in Q5 and Q7, while CR18 compensates for junction drops in Q6 and Q8. Resistors R11 and R12 compensate for the initial charging currents in C 5 and C 6 so that these currents do not flow through R17, R19, CR17 and R18, R20, CR18.

Resistors R17 and R19 as well as R18 and R20 are dividers to develop the $\pm 10 \mathrm{~V}$ reference. The $\pm 10 \mathrm{~V}$ outputs are taken from emitter followers Q7 and Q8.

CR15 and CR16 provide short circuit protection and transistors Q9 and Q10 protect the emitters of Q 7 and Q8 against reverse voltage from shorts between the 10 and 20 volt supplies.

The 10 and 20 volt supplies are regulated and essentially ripple free.

The maximum steady current ratings of the various supplies are:

| Supply | Max Current |
| :---: | :---: |
| $\pm 10 \mathrm{~V}$ | 18 ma |
| $\pm 20 \mathrm{~V}$ | 70 ma |
| $\pm 40 \mathrm{~V}$ | 3 amps |
| $\pm 50 \mathrm{~V}$ | 0.5 amps |

SECTION VI
CIRCUIT DIAGRAMS



ALL RESISTORS 1/8W METAL FILM UNLESS OTHERWISE NOTED.


MODE
FILTER




$$
{ }^{20}
$$

$$
\begin{gathered}
---------------------10 v \\
+10 v \quad+30 v
\end{gathered}
$$

$$
1
$$



NOTES:

* Select for Speaker Protection 2.0A 3AG Maximum Located on Back Poñel.

All Resistors $1 / 8 \mathrm{~W}$ Metal Film Unless Otherwise Noted.
4 - Digit Number by Diodes is Derived from Part Number: CR1 $=1901-0040=1-040$


VIC Power Amplifier
One Channel



$115 \mathrm{~V} / 230 \mathrm{~V}$ CONNECTED FOR 230 V OPERATION

$115 \mathrm{~V} / 230 \mathrm{~V}$ CONNECTED FOR 115 V OPERATION

## VI D2 Primary Circuits

## SECTION VII <br> PARTS LISTS

## A. PHONO PREAMPLIFIER

| Reference Designator | Description | Stock Number |
| :---: | :---: | :---: |
| C1 | 30 pF mica | 0160-2199 |
| C2, C3, C4, C5 | $300 \mu \mathrm{Fnp} 3 \mathrm{~V}$ | 30 D 1614 |
| C6, C7, C8, C9 | $15 \mu \mathrm{~F} 20 \mathrm{~V}$ tantalum | 0180-1746 |
| C10, C11 | $1,000 \mathrm{pF}$ ceramic | 0150-0050 |
| C12 | . $15 \mu \mathrm{~F} 10 \%$ mylar | 0160-0303 |
| CR1, CR2, CR3, CR4, CR5, CR6, CR7, CR8 | silicon diode | 1901-0040 |
| Q1, Q2 | transistor npn X2N4044 | 1854-0221 |
| Q3 | transistor pnp (special) | 1853-0020 |
| Q4 | transistor npn X2N3904 | 1854-0071 |
| Q5 | transistor pnp (special) | 1853-0020 |
| Q6 | transistor npn X2N3904 | 1854-0071 |
| Q7 | transistor pnp (special) | 1853-0020 |
| Q8, Q9 | transistor npn X2N3904 | 1854-0071 |
| Q10 | transistor pnp (special) | 1853-0020 |
| Q11 | transistor npn X2N3904 | 1854-0071 |
| R1* | Value is dependent upon characteristics of the phono pickup used. R1 = 909K for the Shure V-15 Type II. Otherwise calculate R1 per Section III, D. | 0757-019 ** |
| R2 | 20K | 0757-0449 |
| R3 | $1100 \Omega$ | 0757-0424 |
| R4, R5 | $511 \Omega 1 / 8 \mathrm{~W}$ m.f. | 0757-0416 |
| R6 | $10 \Omega$ | 0757-0346 |
| R7, R8 | 100K | 0757-0465 |
| R9 | 46.4K | 0698-3162 |
| R10 | $20 \Omega$ | 0757-0458 |
| R11, R12 | 5.11 K | 0757-0438 |
| R13 | 10K | 0757-0442 |
| R14 | 120 K | 0757-0467 |
| R15 | 26.1 K | 0698-3159 |
| R16 | 56.2 K | 0757-0459 |
| R17 | $200 \Omega$ | 0757-0407 |
| R18 | 10 K | 0757-0442 |
| R19, R20, R21 | $215 \Omega$ | 0698-3441 |
| R22 | 10 K | 0757-0442 |
| R23, R24 | $511 \Omega$ | 0757-0814 |
| R25, R26, R27 | $51.1 \Omega$ | 0757-0394 |
| R28 | 21.5 K | 0757-0199 |
| R29, R30 | 5.11K | 0757-0438 |

B. FILTER BOARD

| Reference Designation | Description | Stock Number |
| :---: | :---: | :---: |
| C1, C2, C3, C4 | . $22 \mu \mathrm{~F}$ mylar | 0170-0086 |
| C5, C6, C7, C8 | $10 \mu \mathrm{~F} 20 \mathrm{~V}$ electrolytic | 0180-0374 |
| C9, C10 | 100 pF mica | 0160-2204 |
| C11, C12 | . $0039 \mu \mathrm{~F}$ mylar | 0160-0166 |
| C13, C14 | . $00125 \mu \mathrm{~F}$ mylar | 0160-0297 |
| C15, C16 | . $018 \mu$ F mylar | 0160-0302 |
| C17, C18 | . $033 \mu$ F mylar | 0160-0163 |
| C19, C20 | . $01 \mu \mathrm{~F}$ mylar | 0160-0161 |
| C21, C22 | . $00125 \mu \mathrm{~F}$ mylar | 0160-0297 |
| C23, C24 | . $68 \mu$ F mylar | 0170-0039 |
| C25, C26 | . 0047 F mylar | 0160-0157 |
| C27, C28 | . $0082 \mu \mathrm{~F}$ mylar (See Schematic VI,B.) | 0160-0160 |
| L1, L2 | Inductor, 31.6 mH | special |
| Q1, Q2, Q3, Q4 | transistor pnp 2N3906 | 1853-0036 |
| Q5, Q6, Q7, Q8 Q9 Q10, Q11, Q12 | transistor npn 2N3904 | 1854-0215 |
| Q13, Q14, Q15, Q16 | transistor pnp 2N3906 | 1853-0036 |
| R1, R2 | 23.7 K | 0698-3158 |
| R3, R4 | 100 K pot | 2100-2516 |
| R5, R6 | 4.7 meg carbon | 0684-4751 |
| R7, R8 | 100K | 0757-0465 |
| R9, R10 | $100 \Omega$ carbon | 0684-1011 |
| R11, R12 | 82.5 K | 0757-0463 |
| R13, R14 | 1.96K | 0698-0083 |
| R15, R16 | 4.7 meg carbon | 0684-4751 |
| R17, R18 | $100 \Omega$ carbon | 0684-1011 |
| R19, R20 | 100K pot | 2100-2516 |
| R21, R22 | 82.5 K | 0757-0463 |
| R23, R24 | 1.96K | 0698-0083 |
| R25, R26 | 4.64 K | 0698-3155 |

C. POWER AMPLIFIER

| Reference Designation | Description | Stock Number |
| :---: | :---: | :---: |
| C1 | . $01 \mu \mathrm{~F}$ ceramic | 0150-0093 |
| C2 | $50 \mu \mathrm{~F} 50 \mathrm{~V}$ electrolytic | 0180-0141 |
| C3 | $100 \mu$ F 6V np | 30D603 |
| C4 | $22 \mu \mathrm{~F}$ tantalum | 0180-0228 |
| C5 | $50 \mu \mathrm{~F} 50 \mathrm{~V}$ electrolytic | 0180-0141 |
| C6 | 120 pF mica | 0160-2205 |
| C7 | . $47 \mu \mathrm{~F}$ | 0170-0064 |
| C8 | . $027 \mu \mathrm{~F}$ | 0170-0066 |
| C9 | 36 pF mica | 0160-2308 |
| C10 | $1,000 \mathrm{pF}$ ceramic | 0150-0050 |
| C11, C12, C13 | $50 \mu \mathrm{~F} 50 \mathrm{~V}$ electrolytic | 0180-0141 |
| CR1, CR2, CR3, CR4, CR5, CR6, CR7, CR8, CR9, CR10, CR11, CR12, CR13 | silicon diode | 1901-0040 |
| L1, L2 | $220 \mu \mathrm{H}$ inductor | 9140-0129 |
| Q1, Q2 | transistor npn 2N5551 | 1854-0474 |
| Q3 | transistor pnp 2N5401 | 1853-0264 |
| Q4 | transistor npn 2N5551 | 1854-0474 |
| Q5 | transitor pnp 2N5401 | 1853-0264 |
| Q6 | transistor npn 2N5551 | 1854-0474 |
| Q7 | transistor pnp 2N5401 | 1853-0264 |
| Q8, Q9 | transistor npn 2N5551 | 1854-0474 |
| Q10 | transistor pnp 2N4036 | 1853-0045 |
| R1 | $51.1 \Omega 1 / 8 \mathrm{w}$ | 0757-0394 |
| R2, R3 | 1.5 meg $1 / 4 \mathrm{w}$ carbon | 06.4-1551 |
| R4, R5 | 50 K pot | 2100-2517 |
| R6, R7 | 10K 1/8 w m.f. | 0757-0442 |
| R8 | $3.16 \mathrm{~K} 1 / 8 \mathrm{w}$ | 0757-0297 |
| R9 | 5.11K $1 / 8 \mathrm{w}$ m.f. | 0757-0438 |
| R10 | 10K $1 / 8 \mathrm{w}$ m.f. | 0757-0442 |
| R11, R12 | $200 \Omega 1 / 8 \mathrm{w}$ m.f. | 0757-0407 |
| R13, R14 | $5.11 \mathrm{~K} 1 / 8 \mathrm{w}$ m.f. | 0757-0438 |
| R15 | $34.8 \mathrm{~K} \mathrm{1/8} \mathrm{w} \mathrm{m.f}$. | 0757-0123 |

C. POWER ANIPLIFIER (Continued)

| Reference Designation | Description | Stock Number |
| :---: | :---: | :---: |
| R16 | $5.11 \mathrm{~K} 1 / 8 \mathrm{w}$ m.f. | 0757-0438 |
| R17 | 20K $1 / 8 \mathrm{w}$ m.f. | 0757-0449 |
| R18 | 10K $1 / 8 \mathrm{w}$ m.f. | 0757-0442 |
| R19 | $5.11 \mathrm{~K} 1 / 8 \mathrm{w}$ m.f. | 0757-0438 |
| R20 | 20K 1/8 w m.f. | 0757-0449 |
| R21 | $5.11 \mathrm{~K} 1 / 8 \mathrm{w}$ m.f. | 0757-0438 |
| R22 | $75 \Omega 1 / 8 \mathrm{w}$ m.f. | 0757-0398 |
| R23 | $909 \Omega 1 / 8 \mathrm{w}$ m.f. | 0757-0422 |
| R24 | 1.96K $1 / 8 \mathrm{w}$ m.f. | 0698-0083 |
| R25 | $100 \Omega 1 / 8 \mathrm{w}$ m.f. | 0757-0100 |
| R26 | $10 \mathrm{~K} 1 / 8 \mathrm{w}$ m.f. | 0757-0442 |
| R27, R28 | 100 $1 / 4$ carbon $10 \%$ | 0684-1011 |
| D. POWER SUPPLY |  |  |
| Reference Designation | Description | Storck Number |
| C1, C2 | $350 \mu \mathrm{~F} 15 \mathrm{~V}$ electrolytic | 0180-2216 |
| C3, C4 | $15000 \mu \mathrm{~F} 50 \mathrm{~V}$ Sprague electrolytic | 6821 Type 36D <br> 153G050CC2A |
| C5, C6, C7, C8 | $100 \mu \mathrm{~F} 15 \mathrm{~V}$ electrolytic | 0180-0061 |
| C9, C10, C11, C12 | 1000 pF ceramic | 0150-0050 |
| CR1, CR2, CR3, CR4 | diode, rectifier 3 amp 100 V | 1901-0200 |
| CR5, CR6, CR7, CR8 | diode, rectifier $3 / 4 \mathrm{amp} 100 \mathrm{~V}$ | 1901-0158 |
| CR9, CR10, CR11, CR12 | diode, silicon | 190-0040 |
| CR13, CR14 | diode, Zener 21.5 V | 1902-3245 |
| CR15, CR16 | diode, Zener 9V | 1902-3149 |
| CR17, CR18 | diode, silicon | 1901-0040 |
| Q1 | transistor pnp 2N4036 | 1853-0045 |
| Q2 | transistor npn 2N2405 | 1854-0352 |
| Q3 | transistor npn X2N3904 | 1854-0071 |
| Q4 | transistor pnp (special) | 1853-0020 |
| Q5 | transistor npn 2N2405 | 1854-0352 |
| Q6 | transistor pnp 2N4036 | 1853-0045 |
| Q7 | transistor npn 2N2405 | 1854-0352 |
| Q8, Q9 | transistor pnp 2N4036 | 1853-0045 |
| Q10 | transistor npn 2N2405 | 1854-0352 |

D. POWER SUPPLY (Continued)

| Reference Designation | Description | Stock Number |
| :---: | :---: | :---: |
| R1, R2 | $10 \Omega$ | 0757-0346 |
| R3, R4 | 26.1 K | 0698-3159 |
| R5, R6, R7, R8 | $562 \Omega 1 / 2$ watt | 0757-0815 |
| R9, R10 | 23.7 K | 0698-3158 |
| R11, R12 | 42.2K | 0698-3450 |
| R13, R14 | 22K | 0684-2231 |
| R15, R16 | 1.96 K | 0698-0083 |
| R17, R18, R19, R20 | 1K | 0757-0280 |
| R21, R22 | $562 \Omega 1 / 2$ watt | 0757-0815 |
| R23, R24, R25, R26 | 10K | 0757-0442 |
| E. DECK PARTS |  |  |
| Reference Designation | Description | Stock Number |
| C1, C2 | . $0047 \mu \mathrm{~F}$ | 0160-0155 |
| C3, C4 | . $01 \mu \mathrm{~F}$ ceramic disc cap | 0150-0093 |
| C5, C6 | . $01 \mu \mathrm{~F}$ mylar 200V | 0160-0161 |
| CR1, CR2 | diodes Motorola MR 841 | 1901-1038 |
| F1 | line fuse |  |
|  | 1.6 A slo-blo for 115 V . 8 A slo-blo for 230 V | $\begin{aligned} & 2110-0005 \\ & 2110-0020 \end{aligned}$ |
| F2, F3 | speaker fuses $2 \operatorname{amp}$ max | 2110-0003 |
| J1 | AC power connector | 1251-2357 |
| J2, J3 | power receptacles | 1251-2073 |
| J4 | line fuse holder | 1400-0084 |
|  | nut | 2950-0038 |
|  | washer | 2190-0068 |
| J5, J6 | fuse clips | 1400-0008 |
| J7 | speaker output jack (mates with P1) | Cinch-Jones S-202-B |
| J8 | phono jack, ring tip sleeve | Switchcraft 12B |
| J9 | phono preamp p.c. connector 18 pin | 1251-0141 |
| J10 | power amplifier p.c. connector 18 pin | 1251-0141 |
| J11 | filter and control p.c. connector 27 pin | 1251-0172 |
| J12 | filter and control p.c. connector 10 pin | 1251-0166 |
| $\begin{aligned} & \text { J13, J14, J15, J16, } \\ & \text { J17, J18 } \end{aligned}$ | input jacks | GC Electronics 33-804 |
|  | fibre washers | 3050-0108 |

E. DECK PARTS (Continued)

From: Dan Lansdon $\quad$ Danc: $\quad$ May 1973
ro: Barney Oliver Amplifier Ownergibser: Corrections to Amplifier Nanual

The following corrections should be made to the Barney Oliver Amplifier Manual.
Page 7-2 C11, C12Part No. should read 0160-0156
Page 7-3 ..... R2, R3Part No. should read 0684-1551
Page 7-4 ..... CR9, 10, 11, 12Part No. should read 1901-0040
R27, R28
Part No. should read 0684-1011
Page 7-6 ..... R10
Part No. should read 0684-4731

## INSURANCE POLICY

To insure the spectacular performance of which this fine instrument is capable, it is respectfully requested that you read the instruction manual very carefully, especially Sections II, III and IV. Certain connections are critical. Unless instructions are followed meticulousty, the system PROBABLY WON'T WORK AND COULD BE DAMAGED. To help you avoid pitfalls already encountered by some users, here are a few tips.
A. Be certain that speaker leads are well insulated, (Beware of ancient "zip cord" which may be partially shorted.)
B. Make sure that leads are well soldered to speaker plugs and that there are no frayed wires or solder bridges between the terminals. (An ohmmeter check is advisable after soldering leads to plugs and before connecting leads to speakers.)
C. Be sure there is no connection between left and right speakers (Some existing systems use a "common" lead.)
D. Be careful to avoid even momentary short-circuiting of the speaker outputs or leads. Short circuits will hlow speaker fuses (located under the black cover on the rear of the amplifier). If in doubt, visually inspect these fuses (not with an ohmmeter).
E. If you hive a shand source other than mond (i.e. tuner, tape unit, audio oscillator, etc.), try it first - in any (or all, in turn) of the following inputs on the rear of the amplifier: TUNER, TAPE, AU. 1, AUX2. Fe sure the input switeh is in a position corresponding to the input which is connected. Also be sure the mode switch is in the S'IEREO NORMAL position.
F. If step D works out, then connect the phono pickup leads (from turntable or changer) to the phono inputs - but first:

1. Be sure the pickup (cartridge) has four independent terminals, with no metal or wire connection between any two terminals or between any terminal and the metallic case of the pickup. (See Section III $\cap$.)
2. Make certain there are separate shielded leads from each side (channel) of the pickup) (cartridge). Be sure the re is no connection between leads for left chennel and right channel. (Some changers use a common shield; this will not work on this amplıfier.) Also be sure the leads and shields are not grounded to the turntable or changer chassis - or to anything else. Some turntables or changers will have to be rewired.
3. Connect the amplifier chassis (thumbscrew on rear panel) to the turntable or changer chassis. In many cases this can be done with a piecc of insulated wire. If you still notice hum when phono input is selected, install an outer shield around (but insulated from) the left and right channe! leads and ground his outer shield (only) to: the amplefier chassis thumbscrew and to the turntable or changer chassis. (See Suction 111 A .)
G. If your phono pickup is other than a Shure V-15 Type II, please sec Section III $B$.
H. If after you have carefully gone through steps $A-G$ together with the admonitions and caveats in the instruction manual, your system still does not work, please try to get some help from an electronic friend in your area. Since this is a G-joboperating on a shoestring, we have no funds for trouble shooting or repair except for major rroblems (defective power transformer, defective attenuator, etc.) The likelihood of such problems is very small; on the other hand, if conscientious efforts at trouble shooting in your area lail to achieve results, please get in touch with Dan Lansdon, -hp - Labs, Palo Alto, Ext. 2706.

[^0]:    *Both channels operating simultaneously at maximum output.
    **Continuous high power operation at less than $8 \Omega$ not recommended. See instruction manual.
    $\dagger$ Hum pickup by phono cartridge may cause this figure to be exceeded.

[^1]:    *Located on chassis. See righthand portion of Power Amplifier Schematic, Section VI, C.

